PRESS-FITTING METHOD AND RECTIPYING DEVICE HAVING PRESS-FITTED MEMBER

CROSS REFERENCE TO RELATED APPLICATION

This application is based on and incorporates herein by reference Japanese Patent Application No. 2002-364485 filed on December 16, 2002.

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FIELD OF THE INVENTION

The present invention relates to press-fitting method and a rectifying device having a press-fitted member.

BACKGROUND OF THE INVENTION

An AC generator generates power by using the driving force transmitted from an engine, charges a battery, and supplies power to various kinds of electronic parts. Reducing the size, the weight and the cost of the AC generator while improving the output power is a critical issue to maintain or improve the competitiveness in the market.

A method for manufacturing a rectifying device for an AC generator is proposed in US Patent Document No. US5,828,564 (JP-A-10-242671). In this method, a rectifying element is press-fitted in a through hole formed in a radiation plate. The rectifying element is fixed and electrically connected to the radiation plate with a simple process. As a result, the manufacturing cost is reduced.

Furthermore, reliability f the rectifying element and

the AC generator using this rectifying element is improved by using this method. If the rectifying element is soldered to the radiating plate, the solder starts melting when the temperature of the rectifying element or the radiation plate exceeds the melting point of the solder. The rectifying element is press-fitted in the radiation plate in this method, and therefore the solder melting problem does not occur.

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However, galling occurs in some materials in a presfitting process in which a base of the rectifying element is press-fitted in the hole formed in the radiation plate. If the base, which is an inserting member, and the radiation plate, which is a receiving member, are made of a copper material, the galling occurs.

when the inserting member is inserted in the hole of the receiving member, an excess is produced between surfaces of the inserting member and the receiving member due to the ductility and the tenacity of copper. The excess is pushed in the inserting direction of the inserting member and hardened as the press-fitting process proceeds because space for releasing the excess is not provided.

when the hardness of the excess becomes higher than the hardness of the inserting member, the inserting member is cracked and its outer periphery partially looses contact with the inner periphery of the receiving member. Namely, a contact area between the outer periphery of the inserting member and the inner periphery of the receiving member decreases. As a result, the tightness of physical and electrical connection

between the inserting member and the receiving member decreases. Furthermore, large stress applied to the inserting member due to the hardened excess affects the productivity in the press-fitting process.

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SUMMARY OF THE INVENTION

The present invention therefore has an object to provide a press-fitting method for press-fitting an inserting member to a receiving member, by which galling is less likely to occur. The present invention has another object to provide a rectifying device in which a rectifying element is press-fitted in a radiation plate by the press-fitting method.

A press-fitting method of the present invention includes forming an engaging hole in a receiving member, forming a groove in an inner periphery of the receiving member, and press-fitting an inserting member in the engaging hole of the receiving member while releasing an excess to the groove.

Further, a press-fitting method of the present invention includes punching an engaging hole in a receiving member having hardness higher than that of a receiving member while creating a hardened inner periphery surface on the receiving member, roughening the hardened inner periphery surface, and press-fitting the inserting member in the engaging hole.

Still further, a press-fitting method of the present invention includes punching an engaging hole in the receiving member while forming a sheared surface and a fractured surface on an inner priphery of the receiving member, forming at

least one groove in the inner periphery, and press-fitting the inserting member in the engaging h le by inserting the inserting member from an end of the receiving member adjacent to the sheared surface.

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The excess is released to the groove during the pressfitting of the inserting member in the receiving member. Thus,
galling due to a hardened excess is less likely to occur, and
physical and electrical connections between the inserting
member and the receiving member is maintained. Furthermore,
stress applied to the inserting member due to the hardened
excess is reduced, and the productivity in the press-fitting
process is maintained.

The inserting member is inserted from the side adjacent to the sheared surface. The hole is more precisely sized on this side than on the other side adjacent to the fractured surface. Thus, the inserting member can be more easily set in the receiving member on this side than on the other side upon the start of the press-fitting.

A rectifying device of the present invention is used for a vehicular AC generator having a stator and a rotor. The rectifying device has a rectifying element for rectifying AC voltage induced in the stator coil of the stator when the rotor is rotated and a radiation plate. The radiation plate has an engaging hole that creates an inner periphery of the radiation plate. The inner periphery of the radiation plate has multiple grooves. The rectifying lement is press-fitted in the engaging hole f the radiation plate.

By using the inserting and receiving members and the press-fitting method, the reliability and productivity of the rectifying device and the vehicular AC generator using the rectifying device are improved.

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BRIEF DESCRIPTION OF THE DRAWINGS

The above and other objectives, features and advantages of the present invention will become more apparent from the following detailed description made with reference to the accompanying drawings. In the drawings:

Fig. 1 is a cross-sectional view of a vehicular AC generator according to first to fifth embodiments of the present invention;

Fig. 2 is a partial view of a positive-side radiation plate according to first and second embodiments;

fig. 3 is a side view of a rectifying element according
to the first to fifth embodiments;

Fig. 4 is a cross-sectional view of the rectifying element and a positive-side radiation plate according to the first embodiment;

Fig. 5 is an enlarged cross-sectional view taken along a V-V line of Fig. 2;

Fig. 6 is a diagram showing the size of peripheral-direction grooves shown in Fig. 5;

Fig. 7 is a partial cross-sectional view showing a modification of the grooves formed in the engaging hole of the positive-electrod sid radiation plate;

Fig. 8 is a partial cross-secti nal view showing another modification of the grooves formed in the engaging hole of the positive-electrode side radiation plate;

Fig. 9 is a partial development elevation showing the inner peripheral surface of the engaging hole of the positive-electrode side radiation plate shown in Fig. 8;

Fig. 10 is a diagram showing a modification of plural grooves shown in Fig. 9; and

Fig. 11 is a development elevation showing the inner peripheral surface of the engaging hole formed in the positive-electrode side radiation plate of a second embodiment.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The preferred embodiments of the present invention will be explained with reference to the accompanying drawings. In the drawings, the same numerals are used for the same components and devices.

[First Embodiment]

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Referring to Fig. 1, an AC generator 1 for a vehicle includes a stator 2, a rotor 3, a brushing device 4, a rectifying device 5, a frame 6, a cover 7, and a pulley 8. The stator 2 has a stator core 21 and a three-phase stator coil 23 wound at a predetermined interval around slots formed in the stator core 21.

The rotor 3 has a field coil 31, pole cores 32, and a rotor shaft 33. The field coil 31 is constructed of an insulated copper wir concentrically wound in a cylindrical

shape. Each pole core 32 has six claw poles and cov rs th field coil 31 from opposite sides. The rotor shaft 33 pass s through the center of the pose cores 32.

An axial-flow type cooling fan 34 is welded to an end face of one of the pole cores 32 located adjacent to the pulley 8. The cooling fan 34 is used for blowing cooling air in the axial direction and in the radial direction. A centrifugal type cooling fan 35 is welded to an end face of the other pole core 32 for blowing cooling air in the radial direction.

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The brushing device 4 having brushes 41, 42 is used for passing exciting current from the rectifying device 5 to the field coil 31. The brushes 41, 42 are pressed against slip rings 36, 37 on the rotational shaft 33, respectively.

The rectifying device 5 rectifies the three-phase AC voltage induced in the three-phase stator coil 23 to a DC voltage. The rectifying device 5 includes a terminal base 51, a positive-side radiation plate 52, a negative-side radiation plate 53, and rectifying elements (inserting members) 54, 55. The terminal base 51 contains electrodes for wiring. The positive-side and the negative-side radiation plates 52, 53 are arranged a predetermined distance away from each other. The rectifying elements 54, 55 are press-fitted in an engaging hole formed by punching in the respective radiation plates (receiving members) 52, 53.

A frame 6 houses the stator 2 and the rotor 3. The rotor 3 is supported so that it can rotat about the rotator shaft

33. The stator 2 is fixed at a position a predetermined distance away from the outer peripheral of the pole cores 32. The frame 6 has cooling-air exit windows 61 and a cooling-air intake window 62. The exit windows 61 are opposed to the stator coil 23 projected in the axial direction from the end face of the stator core 21. The intake window 62 is located at the axial end face of the frame 6. The cover 7 covers parts arranged outside the frame 6 away from the pulley 8, including the brushing device 4, the rectifying device 5 and an IC regulator 12, for protecting the parts.

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The rotor 3 is rotated in the predetermined direction by torque transmitted from the engine (not shown) to the pulley 8 via a belt (not shown). When an exciting voltage is applied to the field coil 31 while the rotor 3 is under rotation, the claw poles of the pole cores 32 are excited. As a result, a three-phase AC voltage is generated in the stator coil 23 and DC voltage is provided at the output terminal of the rectifying device 5.

A method of press-fitting the rectifying element 54 in the positive-side radiation plate 52 will be discussed referring to Figs. 2 through 4. The rectifying element 55 is press-fitted in the negative-side radiation plate 53 in the same manner as the press-fitting of the rectifying element to the positive-said radiation plate 52. Therefore, it will not be discussed.

The radiation plate 52 has an engaging hol 150 in which the rectifying element 54 is press-fitted and by which an

inner p riphery of the radiation plate 52 is created. Grooves 152 are formed in the inner periphery of the radiation plate 52 in a circumferential direction and in a section adjacent to a sheared surface (the upper portion of Fig. 4). The grooves 152 are arranged in circumference or slanted off circumference and apart from each other in the direction that the engaging hole 150 is formed. The grooves 152 are not formed in a section adjacent to a fractured surface (the lower portion of Fig. 4).

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The rectifying element 54 includes a heat sink 250, a semiconductor pellet 252 and a lead 254. The heat sink 250 is a cylindrical metal base of the rectifying element 54 and used as an electrode. It has a knurl portion 256 on its outer periphery and a recess portion 258 at one of its ends. The bottom surface of the recess portion 258 is used as a soldering surface to which the semiconductor pellet 252 is soldered.

The heat sink 250 is made of copper and its surface is plated for soldering and protection from oxidation due to contact with air. The hardness of the heat sink 250, which is equal to 160Hv, is higher than the hardness of the hardened radiation plate 52 around the hole, which is between 140 and 150Hv. One surface of the semiconductor pellet 252 is soldered to the heat sink 250, and the lead 254 is soldered to the other surface of the semiconductor pellet 252.

As shown in Fig. 5, four grooves 152 are formed in the inner periphery of the radiation plate 52 in a portion

adjacent to the side from which the rectifying element 54 is inserted (the lower side in Fig. 5). A depth of ach groove 152 is defined so that a root diameter \$\phi^2\$ of the radiation plate 52 at the bottom of the groove 152 is substantially equal to an outer diameter \$\phi^3\$ of the heat sink 250 as shown in Fig. 6. If an inner diameter \$\phi^1\$ of the engaging hole 150 is set to about 13mm, the outer diameter \$\phi^3\$ is set 0.2mm larger than the inner diameter \$\phi^1\$. The root diameter \$\phi^2\$ is set equal to the outer diameter \$\phi^3\$ (the groove depth of 0.1mm), and the groove width is set to 0.1mm.

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The grooves 152 are formed in the radiation plate 52 that has a thickness of about 4mm. However, more than four grooves 152 may be formed and the grooves 152 may be uniformly arranged in the entire inner peripheral. Furthermore, it is preferable to change the shape and the distance between the grooves 152 as appropriate so that galling is less likely to occur even when the press-fitting process proceeds.

in the positive-side radiation plate 52, the radiation plate 52 is prepared in a predetermined shape. Then, the engaging hole 150 is formed by punching press (engaging hole forming step). The four grooves 152 are formed in the inner periphery of the radiation plate 52 (groove forming step). The rectifying element 54 is press-fitted while an excess produced as the rectifying element 54 is further inserted in the hole 150 is released to the groove 152 (press-fitting step).

The excess is released t the grooves 152 during the

press-fitting of the rectifying element 54 in the hole 150. Moreover, the multiple grooves 152 enable the excess to be dividedly released into different grooves 152. Therefore, the excess does not build up in one place and galling is less likely to occur. Although galling is more likely to occur if both heat sink 250 and the radiation plate 52 are made of copper, the galling is effectively reduced with this configuration.

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Furthermore, the grooves 152 are formed in the inner periphery of the radiation plate 52 apart from each other in the direction that the engaging hole 150 is formed. Since the excess produced along the direction that the rectifying element 54 is press-fitted is dividedly released into the multiple grooves 152, the galling can be reduced.

The grooves 152 are arranged in the inner periphery of the radiation plate 52 and on the side from which the rectifying element 54 is inserted for press-fitting. Thus, the excess produced by the press-fitting of the rectifying element 54 can be dividedly released from the early stage of the press-fitting step.

The root diameter \$2 is set substantially equal to the outer diameter \$3. Therefore, the excess produced by the press-fitting of the rectifying element 54 can be dividedly released into each groove 152. The galling is less likely to occur during press-fitting of the rectifying element 54 into the radiation plate 52 with this configuration. Consequently, the physical and the electrical connections between the

rectifying element 54 and the radiation plate 52 are maintained and the stress caused by the excess is reduced.

[Second Embodiment]

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A groove 154 is formed in a spiral in the inner periphery of the positive-side radiation plate 52 as shown in Fig. 7. The rest of configuration of the radiation plate 52 is the same as the first embodiment. The groove 154 performs the same function as the multiple grooves 152 of the first embodiment. It functions as if it is constructed of multiple grooves with respect to the direction in which the rectifying element 54 is inserted in the radiation plate 52. Thus, an excess produced by the press-fitting of the rectifying element 54 can be dividedly released to the groove 154.

The groove 154 has an advantage over the grooves 152 in the groove forming step. In the groove forming step of the groove 154, only one groove is formed in a series of machine works while multiple series of machine works are required to form the grooves 152. Namely, the groove forming step of the groove 154 is simplified in comparison with that of the grooves 152.

[Third Embodiment]

Referring to Figs. 8 and 9, multiple grooves 156 are formed in the inner periphery of the positive-side radiation plate 52. The grooves 156 are formed in the direction that the engaging hole 150 is formed and apart from each other in the circumfer ntial direction of the radiation plat 52. The rest of configuration is the same as the first embodiment.

An xcess produced during the press-fitting of the rectifying element 54 in the hole 150 is released into th grooves 156. Thus, the excess is less likely to build up and galling between the radiation plate 52 and the rectifying element 54 is reduced. By forming the grooves 156 in the entire inner periphery of the radiation plate 52 as shown in Fig. 8, the excess is effectively released into the grooves 156.

It is preferable that each groove 156 has a depth of about 0.1mm and a width of about 0.1mm. If the inner diameter \$\phi\$1 of the engaging hole 150 is about 13mm, it is preferable that about 40 to 78 grooves 156 are provided so that the necessary contact area for securing the rectifying element 54 in the radiation plate 52 is maintained.

[Fourth Embodiment]

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Referring to Fig. 10, multiple grooves 158 are in the inner periphery of the positive-side radiation plate 52. The grooves 158 are slanted in the circumference direction of the radiation plate 52. With this configuration, an excess produced during the press-fitting of the rectifying element 54 to the radiation plate 52 is dividedly released into the grooves 158.

[Fifth Embodiment]

As shown in Fig. 11, a part of a hardened inner periphery surface of the positive-side radiation plate 52 is roughened.

At least the surface in the area defined by an opening f the engaging hole 150 and a depth L, which is preferably larger

than a thickness of the radiati n plate 52, is roughened. An excess produced by the press-fitting of the rectifying element 54 moves in the direction that the rectifying element 54 is inserted. Thus, the surface adjacent to the opening is preferable to be roughened for effective releasing of the excess. An entire hardened inner periphery surface can be roughened.

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The radiation plate 52 is prepared in a predetermined shape and the engaging hole 150 is punched prior to the press-fitting of the rectifying element 54 (engaging hole forming step). By this engaging hole forming step, a hardened inner periphery surface of the radiation plate 52 is created. The hardened inner periphery surface of the radiation plate 52 is then roughened (surface roughening step). Then, the rectifying element 54 is press-fitted in the direction that the engaging hole 150 is formed (press-fitting step).

In the surface roughening step, the surface is roughened by wire brushing, sanding, or lathe turning. In the wire brushing, the surface is scratched with a wire brush. In the sanding, the surface is sanded with a sand paper. In the lathe turning, the surface is turned by a lathe turning machine. In any cases, flaws having a depth of 10 to 15µm are formed on the surface, and the roughness of the surface becomes equal to or larger than 20Z. The hardness of the surface is reduced to about 80EV, which is substantially equal to the hardness of oth r portions of the radiation plate 52. Galling caused by the excess hardened during the press-fitting the rectifying

lement 54 is reduced. Therefore, the physical and the electrical connections between the rectifying element 54 and the radiation plate 52 are maintained. Moreover, stress due to the excess is reduced.

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The present invention is not limited to the above-described embodiments, and various modifications may be made without departing from the subject matter of the present invention. For example, the inserting member is not limited to a heat sink of a rectifying element. The grooves can be formed in a section of the radiation plate adjacent to the fractured surface.

Forming grooves in the inner periphery of the radiation plate 52 and roughening the hardened inner periphery surface of the radiation plate 52 may be performed in one step. When the heat sink 250 of the rectifying element 54 and the positive-electrode radiation plate 52 are made of a material other than copper, galling can be reduced with the present invention.